

Pumping Dynamics of Cold-Atom Experiments in a Single Vacuum Chamber

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A nonlinear analytical model for the pressure dynamics in a vacuum chamber, pumped with a sputter ion pump (SIP), is proposed, discussed and experimentally evaluated. The model describes the physics of the pumping mechanism of SIPs in the context of a cold-atom experiment. By using this model, we fit pump-down curves of our vacuum system to extract the relevant physical parameters characterizing its pressure dynamics. The aim of this investigation is the optimization of cold-atom experiments in terms of reducing the dead time for quantum sensing using atom interferometry. We develop a calibration method to improve the precision in pressure measurements via the ion current in SIPs. Our method is based on a careful analysis of the gas conductance and pumping in order to reliably link the pressure readings at the SIP with the actual pressure in the vacuum (science) chamber. Our results are in agreement with the existence of essentially two pumping regimes determined by the pressure level in the system. In particular, we find our results in agreement with the well-known fact that for a given applied voltage, at low pressures, the discharge current efficiently sputters pumping material from the pump's electrodes. This process sets the leading pumping mechanism in this limit. At high pressures, the discharge current drops and the pumping is mainly performed by the already sputtered material.

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I. INTRODUCTION

Quantum sensing plays a significant role in the development of the future quantum technologies [1,2]. So far, this sensing technology has been developed on different physical platforms and, in particular, using cold atoms. Among the most relevant realizations one can count atomic microwave and optical clocks [3], magnetometers [4,5], and atom interferometers for inertial sensing [6–9], to mention a few. In fact, their quantum nature offers a very high sensitivity to measure gravity [10–12], fundamental constants [13,14], and general relativity effects [15–17]. Nowadays, these experimental realizations have been developed not only to a metrology level, being operated as standards, but also as instruments with a maturity that allows industrial and commercial applications [18,19].

A key element to reach the required level of sensitivity to a physical phenomenon is the preparation of a well-controlled state of the atoms in terms of their internal and external degrees of freedom. This requires laser cooling in a magneto-optical trap (MOT) to sub-Doppler temperatures (on the order of 1 μ K and below), which unavoidably introduces a dead time in the measurement process. For atom interferometers, this translates into the

well-known Dick effect that degrades the stability of these devices [20–23]. To reduce the MOT loading time, a relatively high background partial pressure of the atoms to be cooled [24] is required, for example, approximately 10^{-8} mbar for ^{87}Rb atoms. However, this high background pressure reduces the available lifetime to perform the desired experiments with the trapped atom clouds [25] and also, it degrades the contrast of the interference fringes leading to a reduction of the signal-to-noise ratio of the measurements.

In a typical cold-atom experiment the high background pressure problem is overcome, on the one hand, by using two chambers connected via a differential pumping stage. In this situation, one chamber (at high pressure) is used as a bright source of cold atoms and the other one (at low pressure) as a science chamber. However, this solution is hardly compatible with the realization of cold-atom-based compact and miniature sensors. So, on the other hand, when using a single vacuum chamber incorporating the atom source (i.e., an alkali metal dispenser) after the MOT loading stage the residual background atoms need to be pumped out quickly. This is needed in order to preserve a useful level of lifetime of the trapped atoms and to avoid an important increase of the dead time. This latter situation implies the ability to switch from high (approximately 10^{-8} mbar) to low pressure (approximately 10^{-11} mbar)

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in a few tenths of ms [26]. A very promising solution has been recently found [27], which allows one to quickly and reversibly control the Rb background pressure in a cell. In this setup, a MOT with up to 10^6 atoms has been realized. However, no compatibility with a pressure level of approximately 10^{-11} mbar has been demonstrated yet with this technique.

Besides the investigations presented in Refs. [26] and [27], other relevant studies on the optimized operation of compact UHV systems have been reported before. In Ref. [28], the authors present a detailed analysis on the use of light-induced atomic desorption to modulate the background pressure of ^{87}Rb atoms in a glass cell. They developed a model to find the number of atoms loaded in a MOT when the light is on, and demonstrated an order of magnitude increase under this condition. In the context of atom interferometry and atom sensors, an UHV system was designed and tested for operation in the highly vibrating environment of a rocket [29]. In Ref. [30], the authors investigated the use of passive vacuum pumps (nonevaporable getter pumps) for the development of compact cold-atom sensors. Finally, in Ref. [31], microfabricated nonmagnetic ion pumps were demonstrated with the aim of maintaining UHV conditions in miniature vacuum chambers for atom interferometry.

The aim of the present work is to understand from the physics point of view, the pressure dynamics of single vacuum chambers loaded with atoms via a dispenser and pumped out by a SIP. So far, SIPs are commonly used in cold-atom experiments requiring UHV. Since they are an unavoidable component, which is at the same time able to provide pressure readings [32,33], it is therefore relevant to have a physical model of the observed vacuum dynamics. This dynamics is not only determined by the pumping mechanism of the SIPs but also by conductance of the whole system and the dispenser sourcing effect. Understanding this dynamics would allow, for instance, the design of miniature SIPs [31] and avoid the use of pressure gauges improving the compactness of the experiments.

To reach a good fidelity in estimating the pressure at the vacuum chamber, we develop an accurate calibration procedure to quantify the leakage ion current in the SIP. To achieve this goal, we first model the conductance of the vacuum system. Then, using the model and a protocol based on a pulsed dispenser current, we measure the temporal evolution of the pressure in the system. As we will see, the physical parameters describing the pressure dynamics extracted in this way, allow the reduction of the dead time in cold-atom experiments by combining a fast loading rate of cold-atom clouds (high partial ^{87}Rb pressure regime) and a fast removal of background atoms after the production of these clouds [26]. It is worth mentioning that the commonly used models [34,35] for the SIP pumping speed do not explain the important pressure variations (more than 2 orders of magnitude) we observe. In fact,

on measurement time scales of several min, the nature of the dominant pumping mechanism changes, and this effect needs to be taken into account.

II. STEADY-STATE PUMPING BEHAVIOR

In this paper, we consider a single-vacuum-chamber system, as represented in Fig. 1. It is a simplified configuration containing a chamber of volume V_1 with the atom source (dispenser) that produces a flow $Q(t)$ that goes to a pump with a nominal pumping speed S . The pump and the chamber are connected through a pipe with a conductance C . With these definitions, we can then relate the pressure at the chamber $P_1(t)$ to the pressure at the pump $P_2(t)$. In a steady state, neglecting leaks and in the free molecular regime, these quantities are related by the equation of the steady-state sourcing flux $Q(\infty)$

$$Q(\infty) = C[P_1(\infty) - P_2(\infty)] = SP_2(\infty) = S_{\text{eff}}P_1(\infty), \quad (1)$$

where S_{eff} is the effective pumping speed seen by the chamber as determined by C . More generally, P_1 follows the gas balance equation [36]

$$V_1 \frac{dP_1(t)}{dt} = Q(t) - S_{\text{eff}}P_1(t). \quad (2)$$

Since the characteristic pumping time $\tau \equiv V_1/S_{\text{eff}}$ controls the pressure transients in the vacuum system, S_{eff} needs to be properly determined. This is an important question in

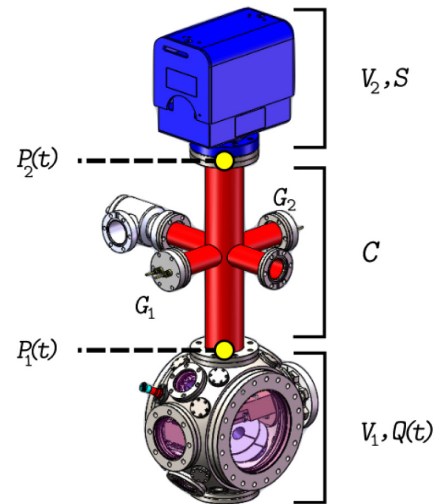


FIG. 1. Sketch of the considered experimental setup. The vacuum chamber of volume V_1 contains the atom source producing a flow $Q(t)$. This gas at a pressure $P_1(t)$ in the chamber produces a pressure $P_2(t)$ at the pump through a pipe of conductance C . In the pump volume V_2 , the atoms are pumped at a nominal speed S . Also represented in this figure are deactivated getter pumps G_1 and G_2 .

particular for cold-atom experiments with time-dependent sources of alkali atoms.

A. Leakage current

Normally, the pressure is translated into current readings by the pump controller. However, in the presence of alkali gases there exists a modification of the pump leakage current I_ℓ [37]. This modification is responsible for an overestimation of the real pressure. It originates from a thin layer of alkali ions stuck to the pump walls. Together with I_ℓ there is also an ion current I produced by the ionization of the gas flowing through the pump electrodes. These two currents contribute to the measured current I_m actually reported by the pump controller (the current reading).

The leakage current I_ℓ is typically on the order of 100 nA and it is usually neglected in high vacuum regimes (it corresponds to an overestimation of $\simeq 10^{-9}$ mbar). However, neglecting this current affects the use of the ion pump as a pressure gauge in the UHV regime [36] ($< 10^{-9}$ mbar). So, we include the effect of this current in the analysis below.

Following ion-pump manufacturers and taking into account that $I = I(P_2)$ is a function of the pressure at the pump, we have the following expression for I_m :

$$I_m(U) = I(P_2) + I_\ell = f(P_2) \times U + I_\ell, \quad (3)$$

where U is the applied voltage between the pump electrodes. From this equation, we see that an accurate determination of the actual pressure (P_2 or I) requires a precise knowledge of the leakage current. The usual way of finding I_ℓ is to measure I_m while the pump's magnets are removed. In this situation, there is no ionization process and we have $I = 0$ A. However, this method requires the pump to be stopped and does not allow a real-time monitoring of the pressure.

Here, we measure I_ℓ by gradually decreasing U within the nominal working range of the pump [37]. Following Eq. (3), the leakage current is then determined by extrapolating the data to $U = 0$ V. The result of this measurement is presented in Fig. 2, where the observed linear behavior indicates that the pressure P_2 does not depend on the applied voltage U at the pressure levels we perform the experiment. The obtained value of the leakage current is $I_\ell = 119.0 \pm 0.4$ nA. As we will see in the following section, the accuracy in the pressure measurement obtained with this method allows us to model the pumping dynamics for pressures $< 10^{-9}$ mbar.

B. Determination of the pressure at the chamber from the SIP current

Once the leakage current is found, we can evaluate the ion current inside the pump $I(P_2)$ using Eq. (3) and the current reading I_m . The next problem is then to determine the explicit dependence of the ion current on the pressure

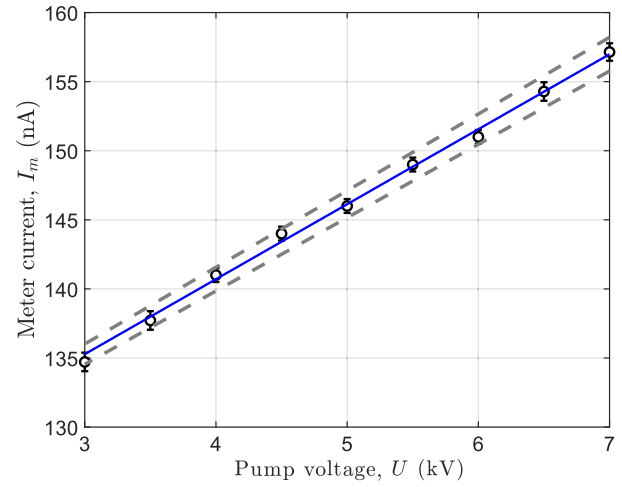


FIG. 2. Current-voltage (I - V) characteristic of the pump. The leakage current $I_\ell = 119.0 \pm 0.4$ nA is obtained from a linear fit (solid line) of the measured current I_m . Dashed lines represent the confidence interval of the fitting parameters.

at the pump, $f(P_2)$. Then we can invert the function $f(P_2)$ and, in the steady-state regime, compute the pressure at the chamber using Eq. (1), namely

$$P_1 = \left(\frac{S}{C} + 1 \right) P_2. \quad (4)$$

In the free molecular regime, the conductance C depends only on the geometry of the vacuum system for a given gas species and temperature. Using the Santeler equation [38] for the transmission probability through a cylindrical pipe of radius R and length L , we can calculate the conductance for a molecule of mass m at room temperature using the relation [36]

$$C = 11.75\pi R^2 \sqrt{\frac{m_{N_2}}{m}} \left\{ 1 + \frac{3L}{8R} \left[1 + \frac{1}{3(1 + L/7R)} \right] \right\}^{-1}. \quad (5)$$

In Eq. (5) m_{N_2} is the mass of a nitrogen molecule, and R and L must be expressed in cm to get C in $L s^{-1}$. Now, let us get an estimate of the value of C for our vacuum system. In a constant-flow regime, the conductance of our particular geometry (central pipe of $L = 35.2$ cm and $R = 3$ cm) evaluates to $C = 32 L s^{-1}$ for the ^{87}Rb monoatomic gas. This value is obtained neglecting contributions from the cross, which is a reasonable assumption in the constant-flow regime. Finding S precisely is slightly more difficult when considering pumping of ^{87}Rb atoms. However, following the pump manufacturer's documentation [37] we can use the linear relation

$$P_2 = \alpha k \frac{I}{U}, \quad (6)$$

to express the pressure at the pump in terms of the ion current. Here, $k = 10.9 \text{ mbar V A}^{-1}$ at room temperature and α is a calibration factor. This factor is the ionization vacuum gauges' correction factor, which links the pressure measurement of specific gas species to calibration measurements using nitrogen. For Rb $\alpha = 4.3$ [39]. As we see later, the empirical relation Eq. (6) does not take into account the fact that the actual relationship between the pressure P_2 and the ion current in the pump I is nonlinear.

With our MOT, we can realize an independent measurement of P_1 instead of computing it using Eq. (4). From the loading curve of the MOT, as shown in Fig. 3, we can find P_1 as indicated in Refs. [40] and [41]. In fact, the loading dynamics of the MOT critically depends on the background pressure of the trapped species and other gases. As has been demonstrated in the past [24,26,40,41], these curves produce reliable pressure measurements. In our experimental setup we use a mirror MOT obtained with an atom chip. The relevant experimental details are as follows: the red-detuned cooling lasers (-1.5Γ where $\Gamma = 2\pi \times 6 \text{ MHz}$ is the natural line width of $^{87}\text{Rb } D_2$ line) have a maximum power of $\simeq 40 \text{ mW}$ shared by four independent MOT beams of about 2.5 cm of $1/e^2$ diameter. The magnetic field gradient is 11 G cm^{-1} . During 100 s of loading, the fluorescence emitted by the atoms is collected on a photodiode with a solid angle of $1.3 \times 10^{-2} \text{ srad}$. This signal is used to compute the atom number. In order to vary the pressure P_1 , we change the dispenser current to produce different stationary gas flows Q .

In analogy to Eq. (6), we assume that the ion current I is proportional to the pressure at the vacuum chamber P_1 , measured with the MOT. That is $I = \beta P_1$, where β is a parameter to be experimentally determined. Then, we can

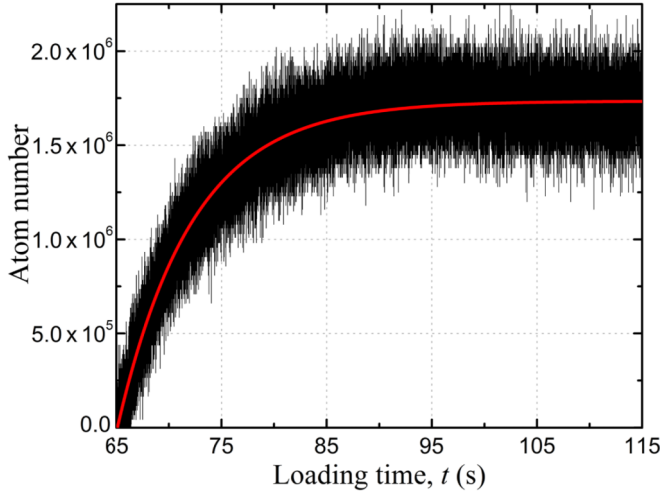


FIG. 3. Number of ^{87}Rb atoms loaded in the MOT (black) for a dispenser current of 4.75 A . The fit (red solid line) to the experimental data gives a characteristic loading time of $7.13 \pm 0.02 \text{ s}$.

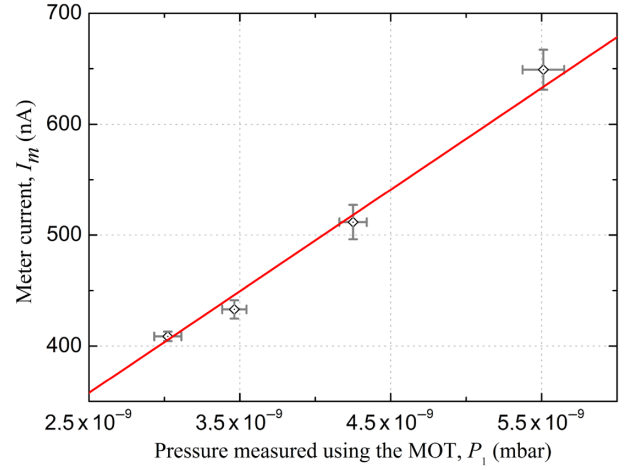


FIG. 4. Meter current versus measured pressure P_1 from MOT loading curves (points). The leakage current I_ℓ and the parameter β extracted from the fit (solid line), using Eq. (7), are respectively equal to $130 \pm 20 \text{ nA}$ and $(9.2 \pm 0.6) \times 10^{10} \text{ nA mbar}^{-1}$.

write the following equation for the ion current reading as a function of the pressure I_m

$$I_m = I_\ell + \beta P_1. \quad (7)$$

In Fig. 4 we plot the dependence of I_m on the pressure P_1 measured from MOT loading curves at steady state. This result offers one independent method to validate the assumption leading to Eq. (7). This method consists in finding the leakage current from MOT measurements and comparing the obtained value with the one extracted from the I - V characterization. Fitting the data in Fig. 4 using Eq. (7), we find for I_ℓ a value of $130 \pm 20 \text{ nA}$, in good agreement with the result given by the I - V characterization presented in Fig. 2. This agreement supports the use of β to compute the pressure in the vacuum chamber by the relation $P_1 = I/\beta$. For the parameter β we obtain the value of $(9.2 \pm 0.6) \times 10^{10} \text{ nA mbar}^{-1}$.

It would be tempting to use the information from Eq. (4) and Eqs. (6) and (7) to find the pumping speed S . However, as we will see in the next section, constant pumping speeds do not properly describe the transient behavior of the pressure when switching on and off the dispenser current.

III. ANALYSIS OF THE NONLINEAR PUMPING DYNAMICS

A. Derivation of the dynamics

When searching for the reduction of the vacuum-system contribution to the dead time between interferometric measurements, we need to focus on the pump-down dynamics that is triggered after loading the MOT and switching off the atom source (dispenser). To achieve this goal, we devise a pressure measurement protocol, which is as follows: first, we switch on the dispenser at a given current

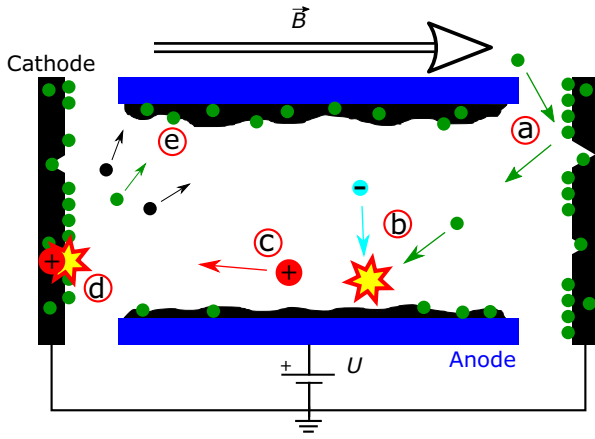


FIG. 5. Representation of the pumping unit cell (of Penning type). A high voltage U is applied between the anode (blue), covered by some getter material (black), and the cathode (black). A gas particle (green) enters the pumping cell and hits the cathode (a) where it is stuck or deflected towards the anode. On its way to this electrode, the particle collides with an electron (b) and gets ionized. The ion is then accelerated towards the cathode (c) with eventually enough energy to be buried and sputter pumping material (d). The freshly sputtered material covers the internal walls of the cylindrical anode (e), which is then ready to pump more particles.

and monitor the pressure rise until it reaches the steady state [41]. The current ranges from 3.75 to 5 A, with a step of 0.25 A. Then, we switch off the dispenser and record the pressure decay (pump-down curve) until it goes back to the steady state. We allow both of the transient processes to last for about 1000 s.

In the following, we develop a mathematical formalism to describe the main physical processes taking place during the pump-down dynamics. Firstly, we assume that the dispenser is no longer sourcing atoms into the chamber after being switched off. In this case, we can consider that the pressure evolution is mainly due to the pumping by the SIP in the presence of a residual outgassing flow $Q(t)$ coming from the vacuum chamber. In steady state, $Q(t)$ is solely given by the thermal outgassing in the system. Secondly, we suppose that the pump contains an ensemble of Penning cells with the geometry sketched in Fig. 5. Thirdly, let us assume that at the time instant t :

1. there already exists some sputtered pumping material (e.g., Ti) that pumps the gas, reducing the pressure by an amount $-aP_2(t)dt$ (process ④ in Fig. 5);
2. some trapped molecules are released by the incident ion flux increasing the pressure by $cI(t)dt$ (process ⑤ in Fig. 5);
3. some pumping material sputtered by the ion flux pumps the gas, reducing the pressure by $-aP_2(t) \times bI(t)dt$ (process ③ in Fig. 5).

In point 1 above, the coefficient a represents the probability rate at which a particle reaching the cathode (made out of a pumping material) sticks to it. Furthermore, when the gas molecules get ionized inside the pump (⑥ in Fig. 5), the applied voltage accelerates the ions (③ in Fig. 5) towards the cathode. If the ions have sufficient energy they can release previously trapped particles (when they collide with the walls) with a desorption rate proportional to c (point 2) and also, they can sputter pumping material with a yield characterized by the coefficient b (point 3).

The physical processes we just described are in agreement with the fact that the pumping speed of the SIP decreases when the pressure decreases. The reason is the decrease of the discharge intensity (current per unit pressure) in this situation. This reduction of the pumping speed depends strongly on the pump parameters such as the applied anode voltage, the magnetic field, and the geometry of the pumping cell.

Collecting together the above-mentioned processes, we arrive at the following differential equation for the pressure evolution at the pump:

$$\frac{dP_2(t)}{dt} = -aP_2(t) - aP_2(t) \times bI(t) + cI(t) + \frac{Q(t)}{V_2}, \quad (8)$$

where V_2 is the pump volume. In the next section we use this model to fit the experimental data and determine the physical parameters defining the nonlinear dynamics.

B. Practical fitting model

Instead of working directly with the pressure Eq. (8), here we derive a practical model that allows a fitting of the experimental data. Our meter outputs current values and therefore, it would be more natural to work with the ion current $I(t)$ rather than the pressure $P_2(t)$. However, the physical processes we just discussed indicate that we cannot use Eq. (6) to relate these quantities. Indeed, $I(t)$ has a nontrivial dependence on the pressure governed by the pressure regime the pump is working in. This fact is encoded by the empirical equation [32]

$$I(t) = hP_2(t)^n, \quad (9)$$

where the exponent n is a real number used to identify the different pressure regimes. It depends on the gas species and the geometry of the pump, and is determined from the fitting procedure. In Eq. (9), h is a time-independent calibration parameter defined by the type and size of the pump.

Inserting Eq. (9) into Eq. (8) we obtain the following equation in terms of the ion current:

$$\frac{dI(t)}{dt} = -\alpha_1 I(t) - \alpha_2 I(t)^2 + [\alpha_3 I(t) + q] I(t)^{1-(1/n)}, \quad (10)$$

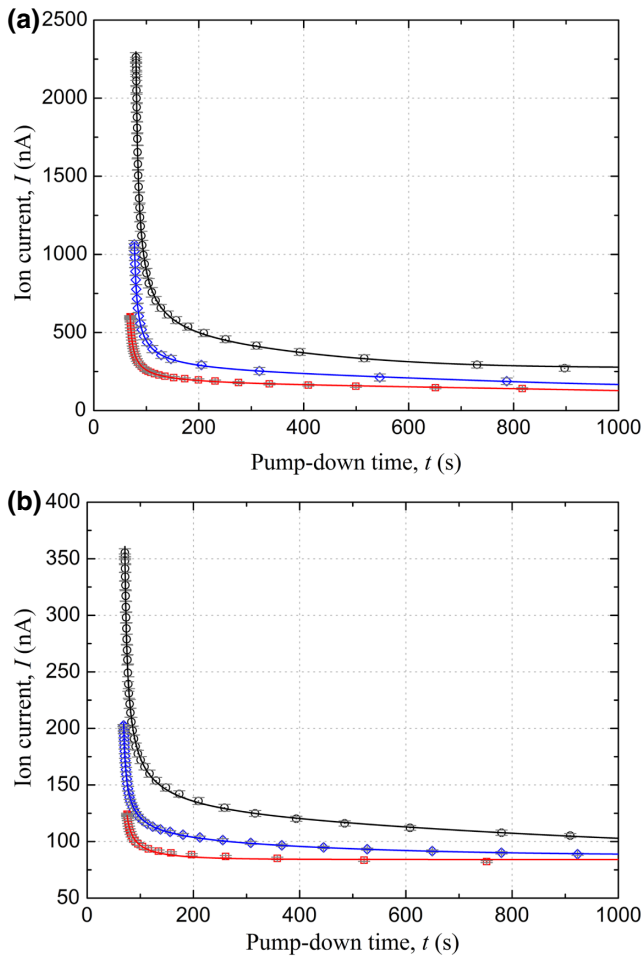


FIG. 6. We record the pump-down curves (data points) after switching off the dispenser currents, initially at levels given in captions (a),(b). In each case, the measured ion current $I(t)$ is fitted (solid lines) by numerical integration of Eq. (10). (a) Dispenser currents are 5 A (black circles), 4.75 A (blue diamonds), and 4.5 A (red squares). (b) Dispenser currents are 4.25 A (black circles), 4 A (blue diamonds), and 3.75 A (red squares).

with $\alpha_1 \equiv na$, $\alpha_2 \equiv nab$, $\alpha_3 \equiv nc\sqrt{h}$, $q \equiv n\sqrt{h}Q_{th}/V_2$. These parameters are treated as independent and used in the fitting procedure. When writing Eq. (10) we consider that after switching off the dispenser, $Q(t)$ reaches the constant thermal outgassing flux Q_{th} in a time scale shorter than the time frame required to reach the steady state. As we will see later, such an approximation is compatible with our observations. We measure the pump-down curves presented in Fig. 6. The points are the experimental data and the solid lines are fits obtained with Eq. (10). As can be seen in this figure, there is a very good agreement between the theory and the experimental data.

To validate the model beyond the criteria set by the fit quality, we study the dependence of the fitting parameters on the pressure P_2 looking at their behavior in different pressure regimes. The measurement protocol used is as

follows: we change the dispenser current and wait until the pressure reaches an equilibrium state. Next, we measure the ion current at this equilibrium situation, before switching off the dispenser. Finally, we start the measurement of the pump-down dynamics. The results obtained with this protocol are presented in Fig. 7. It shows the dependence of the fitting parameters on the initial ion current.

As expected, the value of n increases when the pressure goes down [42] as can be seen in Fig. 7(a). Moreover, it reaches unity at the highest measured pressure. The obtained value in this latter case is actually compatible with pump manufacturers' reported values for air. At low pressures it goes beyond 1.5, a value never reported before to our knowledge and that might be in agreement with the fact that we are pumping an alkali gas.

The parameter a , according to our model, depends on the pump's cathode geometry and the sticking factor, this latter being a function of the temperature and the gas species. From the measurement in Fig. 7(b) we see that at low initial ion currents (pressures) a is relatively constant. This is expected since in this case the sticking probability should correspond to a linear process given the gas density in the pump. However, when the initial ion current is increased, a eventually increases, suggesting a modification of the sticking probability. This is coherent with the fact that in this situation the behavior of n also indicates a change in the pressure regime. We attributed the change of a with the initial ion current to the change in the sticking probability because the cell geometry does not change.

From Fig. 7(c) we see that the parameter b tends to zero when the initial ion current is increased. This is also an expected behavior since this parameter is related to the discharge current, which is depressed by the space-charge effect when the pressure rises. As a consequence, the sputtering rate becomes reduced [32]. In fact, what happens is that at relatively high initial ion currents or pressures, the energy of the ions hitting the cathode is no longer exclusively defined by the applied voltage U .

In order to interpret the behavior of the parameters c and Q_{th} we need to isolate them from the calibration factor h . This requires us to perform independent measurements. However, it is fair to consider h as a scaling factor in Figs. 7(d) and 7(e). In this situation, the increase of c with the initial ion current might be a consequence of the bombardment boost in the presence of a significant number of gas particles in the pump volume. This process naturally leads to a relatively higher desorption rate of buried molecules. Increasing the initial ion current also leads to an increase in the thermal outgassing flux Q_{th} in the time scale we record the data (approximately 1000 s). This effect is already observable in Fig. 6 where the steady-state ion-current value depends on the dispenser current.

Finally, the pressure in the chamber can be determined using the coefficient β obtained from the calibration measurement in Fig. 4 and the expression $P_1(t) = I(t)/\beta$. This

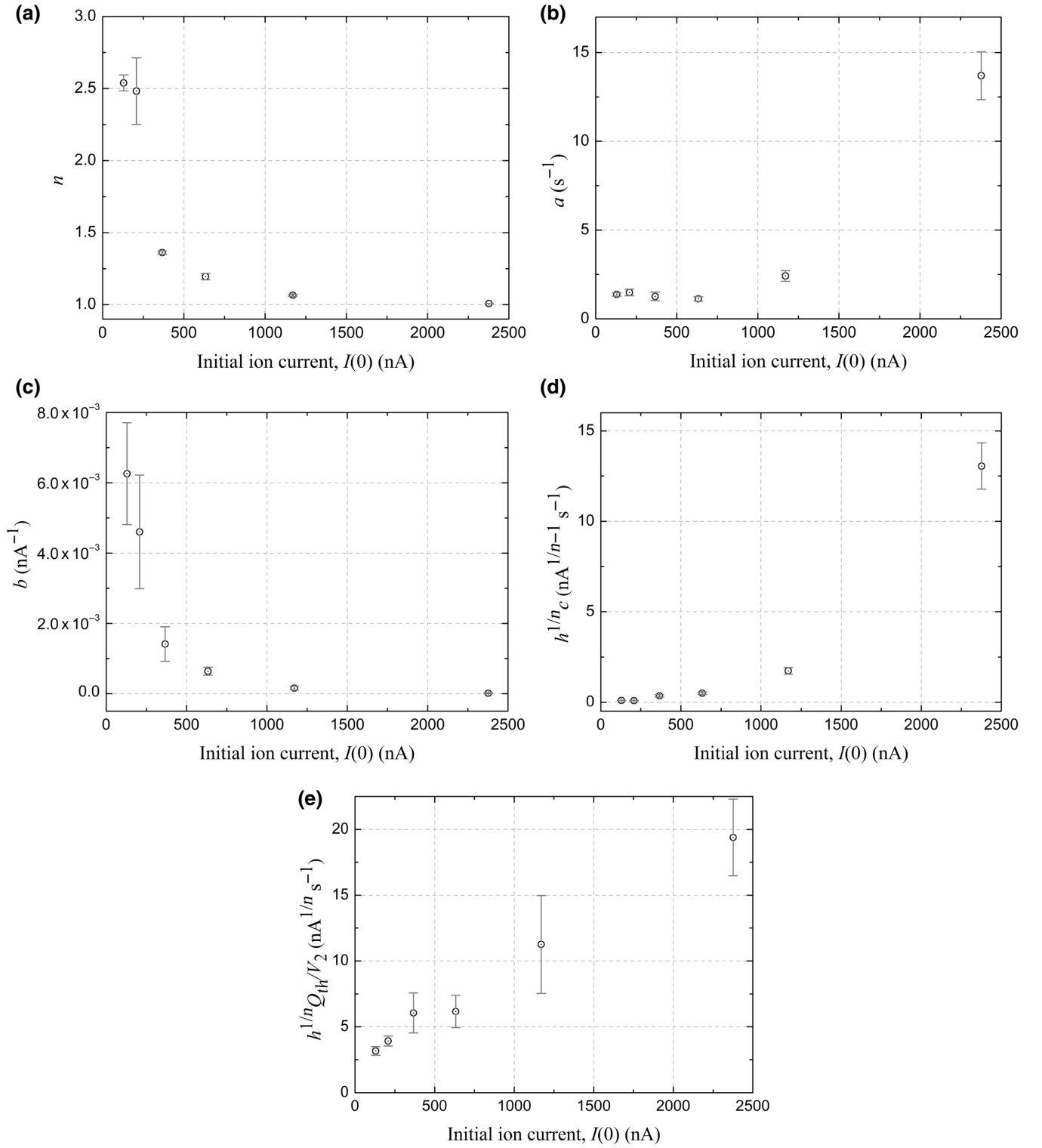


FIG. 7. Dependence of the parameters describing the physical processes in the pump volume on the initial ion current (just after turning off the dispenser current). These parameters result from the fitting of the pump-down curves in Fig. 6 using the numerical solution of the differential Eq. (10). (a) Pumping regime parameter. (b) Former sputtered-material pumping-rate parameter. (c) Instantaneous ion-flux-induced sputtering-pumping-rate parameter. (d) Ion-flux desorption parameter. (e) Thermal outgassing source parameter.

linear relation indicates that the science chamber, at pressure $P_1(t)$, acts as a *passive* particle reservoir feeding the ion current $I(t)$. In contrast, Eq. (9) indicates that the pump volume, at a pressure $P_2(t)$, can be seen as an *active* particle reservoir feeding $I(t)$ because of the physical processes involving the gas inside the pump.

Having these ideas in mind, we can outline the next calibration and monitoring protocols for the time evolution of the pressure in the vacuum chamber.

(a) Calibration protocol

1. Use the MOT to perform a steady-state calibration measurement as in Fig. 4.
2. From the calibration step 1 and Eq. (7) find β .
3. Measure pump-down curves as in Fig. 6 for different initial ion currents $I(0)$.
4. Using Eq. (10), fit the pump-down curves to find the ion current $I(t)$.
5. Find the physical parameters of this model for the different $I(0)$ and fit the data in Fig. 7.

(b) Monitoring protocol

1. In a given experimental run, and before launching the relevant measurement, find $I(0)$.
2. Compute the corresponding physical parameters from the fits done on Fig. 7.
3. Use β from step 2 and the solution $I(t)$ from step 4 to compute the pressure in the chamber as $P_1(t) = I(t)/\beta$.

IV. CONCLUSION

In this work, we developed a detailed physical model of the nonlinear pressure dynamics in sputter ion pumps. This model is experimentally corroborated by the measured data. It includes parameters describing the complex physical processes taking place inside the vacuum pump. Moreover, we characterize the system conductance and use pressure measurements with a MOT to establish a link between the pressure in the vacuum chamber and the ion current provided by the pump. From a practical point of view, this relationship allows the pump current to be used as a good indicator of the pressure in the science chamber. From the observed dynamics, we can tailor the effective pumping speed and optimize the MOT loading time with respect to the contradictory requirements of having high repetition rates and high number of atoms in a single chamber. We hope that the physics investigated in this work will be useful in the future to engineer miniature and microscopic scale ion pumps [31] for cold-atom-based compact quantum sensors.

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